

MIXED PLANE BOUNDARY VALUE PROBLEM OF THE THEORY OF ELASTICITY FOR A QUADRANT

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The problem can be reduced to an integral equation determining shear stresses at a clamped edge. The resulting solution makes it possible to supplement the results of investigation [1,2,3].

Let us study the stress problem in an elastic quadrant $x > 0, y > 0$ in the plane of variable $z = x + iy$ under the action of a concentrated force $Q + iP$, applied at the point $z_0 = x_0 + iy_0$ ($x_0 > 0, y_0 > 0$). Let us assume that when $y = 0$ the displacements v, u are equal to zero, and when $x = 0$ the external loading are equal to zero (Fig. 1).

For the solution of the problem let us complete the quadrant to form a half-plane $x > 0$. Let us load symmetrically the new quadrant $x > 0, y < 0$ at the point $z_0 = x_0 - iy_0$ with a force $Q - iP$. Let us also introduce an additional, temporarily arbitrary loading $q(x)$ distributed along the x -axis. Evidently, under the action of symmetrical loadings $Q + iP, Q - iP$ and $q(x)$ on the half-plane $x > 0$ when $y = 0$,

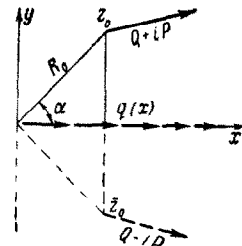


Fig. 1.

the displacement v is equal to zero. The loading $q(x)$ will be determined in such a way as to fulfil the condition $u = 0$ on the x -axis.

Let us study the state of stress of the given half-plane $x > 0$ with free edge $x = 0$ resulting from loadings $Q + iP, Q - iP$ and $q(x)$.

If for the stresses we make use of known representation,

$$\begin{aligned} X_x + Y_y &= 2[\Phi(z) + \overline{\Phi(\bar{z})}] \\ Y_y - X_x + 2iX_y &= 2[\bar{z}\Phi'(z) + \Psi(z)] \end{aligned} \quad (1)$$

then for a general case when the force $P + iQ$ is applied at the point $z_0 = x_0 + iy_0$ according to the formulas* of the paper [5] it is possible to obtain

$$\Phi_1(Q + iP, z, z_0) = -\frac{Q + iP}{2\pi(1 + \kappa)} \left(\frac{1}{z - z_0} + \frac{\kappa}{z + \bar{z}_0} \right) - \frac{Q - iP}{2\pi(1 + \kappa)} \frac{z_0 + \bar{z}_0}{(z + \bar{z}_0)^2} \quad (2)$$

$$\Psi_1(Q + iP, z, z_0) = \frac{Q - iP}{2\pi(1 + \kappa)} \left[\frac{\kappa}{z - z_0} + \frac{1}{z + \bar{z}_0} + \frac{z_0 + \bar{z}_0}{(z + \bar{z}_0)^2} \right] - \frac{z}{z_0} \frac{d\Phi_1}{dz} \quad \left(\kappa = \frac{3 - \nu}{1 + \nu} \right)$$

In the case when loadings $Q + iP$, $Q - iP$ and $q(x)$ are acting on the half-plane, we will obtain

$$\Phi(z) = \Phi_1(Q + iP, z, z_0) + \Phi_1(Q - iP, z, \bar{z}_0) + \int_0^{\infty} \Phi_1[q(t), z, t] dt \quad (3)$$

$$\Psi(z) = \Psi_1(Q + iP, z, z_0) + \Psi_1(Q - iP, z, \bar{z}_0) + \int_0^{\infty} \Psi_1[q(t), z, t] dt$$

If $q(x)$ is determined from the condition $u = 0$ when $y = 0$, then the formulas (3) and (1) with $x > 0$, $y > 0$ will provide the solution of the problem for the stresses in an elastic quadrant with the assigned boundary conditions.

The condition $u = 0$ when $y = 0$, except for a rigid body displacement and taking into account that solution (3) satisfies the condition $v = 0$ when $y = 0$, is equivalent to the condition $u_x + iv_x = 0$. If representations (1) are made use of, the latter can be expressed as

$$\kappa\Phi(x) - \overline{\Phi(x)} - x\overline{\Phi'(x)} - \overline{\Psi'(x)} = 0 \quad (4)$$

Subjecting the functions $\Phi(z)$ and $\Psi(z)$ to be condition (4), we will obtain a singular integral equation for $q(x)$

$$2\kappa \int_0^{\infty} \frac{q(t)}{t - x} dt - \int_0^{\infty} \left[\frac{1 + \kappa^2}{t + x} + \frac{4t(x - t)}{(t + x)^3} \right] q(t) dt = \quad (5)$$

$$= (Q + iP)F(x, z_0) + (Q - iP)F(x, \bar{z}_0)$$

where

$$F(x, z_0) = \frac{x}{x - z_0} + \frac{z_0 - \bar{z}_0}{(x - z_0)^2} + \frac{x}{x - \bar{z}_0} + \frac{1}{x + z_0} + \frac{x(z_0 + \bar{z}_0)}{(x + z_0)^2} -$$

$$- \frac{2(z_0 - x)(z_0 + \bar{z}_0)}{(x + z_0)^3} + \frac{x^2}{x + \bar{z}_0} - \frac{2x\bar{z}_0}{(x + \bar{z}_0)^2}$$

* In deducing expression (2), an error was corrected in one of the formulas of paper [5].

Let us normalize equation (5), assuming

$$\frac{1}{\pi i} \int_0^{\infty} \frac{q(t)}{t-x} dt = \frac{r(x)}{\sqrt{x}} \tag{6}$$

With consideration of integrability of function $q(x)$, we have the transformation [4]

$$q(x) = \frac{1}{\pi i \sqrt{x}} \int_0^{\infty} \frac{r(t)}{t-x} dt \tag{7}$$

Introducing into equation (5) expressions (6) and (7) and changing the order of integration while taking into account that

$$\int_0^{\infty} \frac{dt}{\sqrt{t}(t+x)(t_1-t)} = \frac{\pi}{\sqrt{x}(x+t_1)}$$

$$\int_0^{\infty} \frac{t(x-t) dt}{\sqrt{t}(t_1-t)(t+x)^3} = -\frac{\pi \sqrt{x}}{4x(x+t_1)^3} (x^2 - 6xt_1 + t_1^3)$$

we obtain the equation for the function $r(x)$

$$r(x) + \frac{x}{2\pi} \int_0^{\infty} \frac{r(t)}{x+t} dt + \frac{4}{x\pi} \int_0^{\infty} \frac{tx}{(t+x)^3} r(t) dt =$$

$$= \frac{\sqrt{x}}{2\pi i} [(Q + iP) F(x, z_0) + (Q - iP) F(x, \bar{z}_0)] \tag{8}$$

Assuming that $t = e^\tau$, $x = e^\xi$, $r(x) = \psi(\xi)$, we can express equation (8) in the form

$$\psi(\xi) + \frac{x}{2\pi} \int_{-\infty}^{\infty} \frac{\psi(\tau) d\tau}{1 + e^{\xi-\tau}} + \frac{4}{x\pi} \int_{-\infty}^{\infty} \frac{e^{\xi-\tau}}{(1 + e^{\xi-\tau})^3} \psi(\tau) d\tau =$$

$$= \frac{\sqrt{e^\xi}}{2\pi i} [(Q + iP) F(e^\xi, z_0) + (Q - iP) F(e^\xi, \bar{z}_0)] \tag{9}$$

Applying to both sides of the equation (9) the Laplace transform and using the notation

$$R(p) = \int_{-\infty}^{\infty} \psi(\xi) e^{-p\xi} d\xi$$

we obtain

$$R(p) \left[1 + \frac{x}{2\pi} \int_{-\infty}^{\infty} \frac{e^{-p\theta} d\theta}{1 + e^\theta} + \frac{4}{x\pi} \int_{-\infty}^{\infty} \frac{e^{(1-p)\theta} d\theta}{(1 + e^\theta)^3} \right] =$$

$$= \frac{1}{2\pi i} \int_{-\infty}^{\infty} [(Q + iP) F(e^\xi, z_0) + (Q - iP) F(e^\xi, \bar{z}_0)] e^{(1-p)\xi} d\xi \tag{10}$$

For the integrals of the left and right sides of the equation we have

$$\int_{-\infty}^{\infty} \frac{e^{-p\theta}}{1+e^\theta} d\theta = -\frac{\pi}{\sin \pi p}, \quad \int_{-\infty}^{\infty} \frac{e^{(1-p)\theta}}{(1+e^\theta)^3} d\theta = \frac{p(p+1)}{2} \frac{\pi}{\sin \pi p}$$

$$\int_{-\infty}^{\infty} \frac{e^{(1/2-p)\xi}}{e^\xi - z_0} d\xi = \frac{\pi i e^{i\pi p}}{\cos \pi p} z_0^{-p-1/2}, \quad \int_{-\infty}^{\infty} \frac{e^{(1/2-p)\xi}}{(e^\xi - z_0)^2} d\xi = -\frac{\pi i e^{i\pi p}}{2 \cos \pi p} (2p+1) z_0^{-p-1/2}$$

$$\int_{-\infty}^{\infty} \frac{e^{(1/2-p)\xi}}{(e^\xi - z_0)^3} d\xi = \frac{\pi i e^{i\pi p}}{8 \cos \pi p} (2p+1)(2p+3) z_0^{-p-1/2}$$

Here $-1/2 < \text{Re } p < 0$. We can now write equation (10) as

$$R(p) \left[1 - \frac{\kappa}{2 \sin \pi p} + \frac{2}{\kappa} \frac{p(p+1)}{\sin \pi p} \right] =$$

$$= \frac{e^{\pi i p}}{2\kappa \cos \pi p} \{ (Q + iP) F_1(p, z_0) + (Q - iP) F_1(p, \bar{z}_0) \} \tag{11}$$

Here

$$F_1(p, z_0) = \kappa z_0^{-p-1/2} - (z_0 - \bar{z}_0) \left(p + \frac{1}{2} \right) z_0^{-p-3/2} + \kappa \bar{z}_0^{-p-\frac{1}{2}} + (-z_0)^{-p-1/2} -$$

$$- \kappa (z_0 + \bar{z}_0) \left(p + \frac{1}{2} \right) (-z_0)^{-p-3/2} + 2(z_0 + \bar{z}_0) \left(p + \frac{1}{2} \right)^2 (-z_0)^{-p-5/2} + \kappa^2 (-\bar{z}_0)^{-p-1/2} +$$

$$+ 2\kappa \bar{z}_0 \left(p + \frac{1}{2} \right) (-\bar{z}_0)^{-p-3/2}.$$

Introducing $z_0 = R_0 e^{i\alpha}$ ($0 < \alpha < 1/2\pi$), from equation (11) we obtain

$$R(p) = \frac{2i \operatorname{tg} \pi p T(p)}{2\kappa \sin \pi p - \kappa^2 + 4p(p+1)} R_0^{-p-1/2} \tag{12}$$

where

$$T(p) = 2Q\kappa \sin \left[\pi p - \alpha \left(p + \frac{1}{2} \right) \right] +$$

$$+ Q \left\{ -2 \left(p + \frac{1}{2} \right) \sin \alpha \sin \left[\pi p - \alpha \left(p + \frac{3}{2} \right) \right] - \cos \left(p + \frac{1}{2} \right) \alpha + \right.$$

$$+ 2 \left(p + \frac{1}{2} \right) \left[2 \left(p + \frac{1}{2} \right) - \kappa \right] \cos \alpha \cos \left(p + \frac{3}{2} \right) \alpha + \kappa \left[2 \left(p + \frac{1}{2} \right) - \kappa \right] \cos \left(p + \frac{1}{2} \right) \alpha \Big\} +$$

$$+ P \left\{ 2 \left(p + \frac{1}{2} \right) \sin \alpha \sin \left[\pi p - \alpha \left(p + \frac{3}{2} \right) \right] - \sin \left(p + \frac{1}{2} \right) \alpha + \right.$$

$$+ 2 \left(p + \frac{1}{2} \right) \left[2 \left(p + \frac{1}{2} \right) - \kappa \right] \cos \alpha \sin \left(p + \frac{3}{2} \right) \alpha - \kappa \left[2 \left(p + \frac{1}{2} \right) - \kappa \right] \sin \left(p + \frac{1}{2} \right) \alpha \Big\}$$

Applying inverse transformation, we find that

$$\psi(\xi) = \frac{1}{2\pi i} \int_{\sigma-i\infty}^{\sigma+i\infty} \frac{2i \operatorname{tg} \pi p T(p)}{2\kappa \sin \pi p - \kappa^2 + 4p(p+1)} R_0^{-p-1/2} e^{p\xi} dp \quad \left(-\frac{1}{2} < \sigma < 0 \right) \tag{13}$$

Introducing $x = e^\xi$, $r(x) = \psi(\xi)$, and referring to equation (7), taking into consideration that

$$\frac{1}{\pi} \int_0^{\infty} \frac{t^p}{t-x} dt = -\frac{x^p}{\operatorname{tg} \pi p}$$

we obtain

$$q(x) = -\frac{1}{\pi i} \int_{\alpha-i\infty}^{\alpha+i\infty} \frac{R_0^{-p-1/2} x^{p-1/2} \Gamma(p)}{2\kappa \sin \pi p - \kappa^2 + 4p(p+1)} dp$$

It is convenient to introduce $s = p + 1/2$ as the variable of integration. Then, as a final result, we will have

$$q(x) = -\frac{1}{\pi i x} \int_{\gamma-i\infty}^{\gamma+i\infty} \frac{S(s)}{4s^2 - 2\kappa \cos \pi s - (1 + \kappa^2)} \left(\frac{x}{R_0}\right)^s ds \quad \left(0 < \gamma < \frac{1}{2}\right) \quad (14)$$

where

$$S(s) = -2Q\kappa \cos(\pi - \alpha)s + Q\{-2s \sin \alpha \sin[\pi s - \alpha(s+1)] - \cos \alpha s + 2s(2s - \kappa) \cos \alpha \cos(s+1)\alpha + \kappa(2s - \kappa) \cos \alpha s\} + P\{-2s \sin \alpha \cos[\pi s - \alpha(s+1)] - \sin \alpha s + 2s(2s - \kappa) \cos \alpha \sin(s+1)\alpha - \kappa(2s - \kappa) \sin \alpha s\}$$

While computing integrals, when $x < R_0$, the calculations are taken from the right, and when $x > R_0$ from the left side of the straight line γ . In particular, when $x < R_0$, we have

$$q(x) = \frac{1}{x} \sum_k \left(\frac{x}{R_0}\right)^{\rho_k} \left[\operatorname{Re} \Omega_k \cos\left(\theta_k \ln \frac{x}{R}\right) - \operatorname{Im} \Omega_k \sin\left(\theta_k \ln \frac{x}{R}\right) \right] \quad (15)$$

where

$$\Omega_k = \frac{S(s_k)}{\kappa \pi \sin \pi s_k + 4s_k}, \quad s_k = \rho_k + i\theta_k \quad \left(\rho_k > 0, 0 < \theta_k < \frac{1}{2} \pi\right)$$

and S_k are the roots of equation

$$4s^2 - 2\kappa \cos \pi s - (1 + \kappa^2) = 0 \quad (16)$$

As equation (16) always has a root for which $\rho < 1$, it is possible to draw the conclusion that when $X_y = 1/2 q(x)$, a corner of the elastic quadrant is approached, the stress, in absolute value, keeps increasing to infinity, while simultaneously changing its sign an infinite number of times.

If we assume that $s = 2\lambda + 1$, then equation (16) will coincide with the equation for determination of order of stress increase in the proximity of the angle. The latter equation was obtained in paper [1].

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